

contact, diode D_3 , and the limit switch, LS-. You need the diode to avoid feeding voltage to the -Limit input through the activated LS+ limit switch. The motor now runs in the opposite direction until the limit switch LS- activates. At that instant, the driver is disabled (for the

negative direction), and relay K_1 turns off. The cycle begins anew.

The values of the components the circuit uses depend principally on the selected servoamplifier and motor, thus **Figure 1** shows no values. The machine has worked satisfactorily in two shifts for more than two years. During this period,

contrary to our expectations, we never readjusted the servoamplifier.

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Linear power driver works from single supply

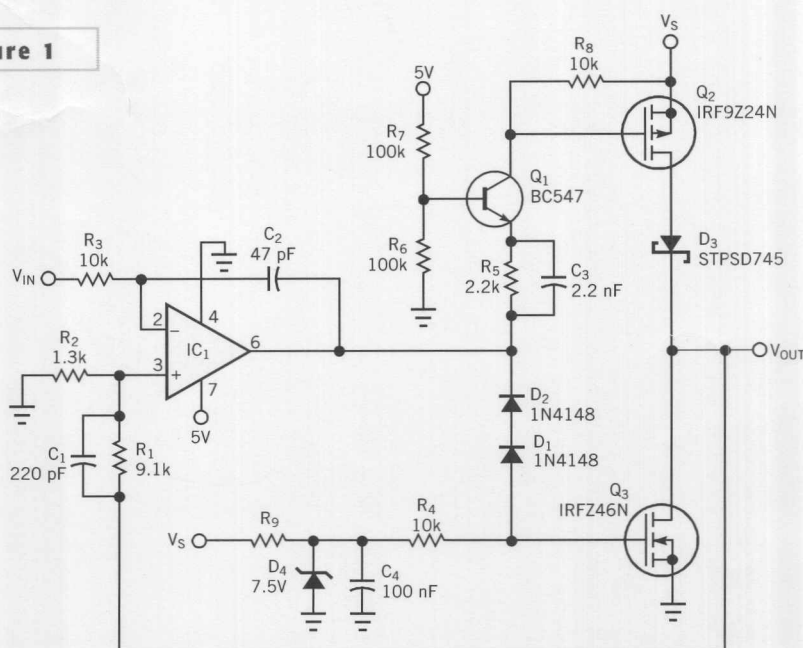
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IN LOW-POWER, single-supply analog applications, it is often desirable to main-

tain precise control of voltages much greater than the positive-supply rail. The circuit in **Figure 1** allows you to amplify the input voltage, V_{IN} , by a factor, A , which resistors R_1 and R_2 set. The output voltage, V_{OUT} , equals AV_{IN} , where $A=R_2/(R_1+R_2)$. The op amp receives its supply from a single 5V source, and the discrete output stage operates from a rectified voltage, V_S , from a power source that meets the requirements of the application. When the circuit neither sinks nor sources current, the op amp's output settles to a voltage higher than 1.9V (Q_1 is completely off) but lower than the threshold voltage of the n-channel FET, Q_3 , minus 1.2V (two diode drops). When V_{IN} rises from a given state, the op amp's output voltage drops and gradually turns on Q_1 . This action results in a voltage drop across R_8 , turning on Q_2 . This process continues until the voltages at the op amp's two inputs match. A decreasing V_{IN} causes the op amp's output voltage to rise to the point at which Q_3 conducts enough to pull down V_{OUT} . Capacitors C_1 , C_2 , and C_3 are necessary to prevent oscillation.

The circuit, useful as a power driver for pulse generators, offers rise and fall times of less than 15 μ sec, virtually independently of the supply voltage, V_S . You can test the design with op amps LMC7101,

Figure 1



This simple circuit allows you to control voltages far in excess of the positive-supply rail.

LT1013, and AD8551. All these op amps deliver load currents as high as 5A at voltages as high as $V_S=40$ V. One important feature of the design is its insensitivity to component tolerances. The values for R_1 and R_2 in **Figure 1** yield $A=8$. The value of R_5 depends on V_S . You could use a logic-level FET, such as the IRLZ34N for Q_3 ; you can then omit the components D_1 , D_2 , D_4 , R_4 , R_9 , and C_4 . In this case, the op amp's output connects directly to the gate of Q_3 , and you must reduce the value of R_6 to lower the base voltage of Q_1 to

maintain the "idle window" in which both Q_1 and Q_3 are off. The op amp's input-voltage range must include ground. D_3 is necessary only in cases in which sources connect to the output. D_3 prevents reverse current flow from the external source through Q_2 . Such a situation can arise when the circuit serves in a battery-charger application.

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